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1	Demonstration of a Three-Dimensional Dynamically Adaptive Atmospheric
2	Dynamic Framework for the Simulation of Mountain Waves
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20 Abstract

21 In this paper, Fluidity-Atmosphere, representative of a three-dimensional (3D) nonhydrostatic Galerkin compressible 22 atmospheric dynamic framework, is generated to resolve large-scale and small-scale phenomena simultaneously. This 23 achievement is facilitated by the use of nonhydrostatic equations and the adoption of a flexible 3D dynamically 24 adaptive mesh where the mesh is denser in areas with higher gradients of variable solutions and relatively sparser in 25 the rest of the domain while maintaining promising accuracy and reducing computational resource requirements. The 26 dynamic core is formulated based on anisotropic tetrahedral meshes in both the horizontal and vertical directions. The 27 performance of the adaptive mesh techniques in Fluidity-Atmosphere is evaluated by simulating the formation and 28 propagation of a nonhydrostatic mountain wave. The 2D anisotropic adaptive mesh shows that the numerical solution 29 is in good agreement with the analytic solution. The variation in the horizontal and vertical resolutions has a strong 30 impact on the smoothness of the results and maintains convergence even at high resolutions. When the simulation is 31 extended to 3D, Fluidity-Atmosphere shows stable and symmetric results in the benchmark test cases. The flows over 32 a bell-shaped mountain are resolved quite smoothly. For steep mountains, Fluidity-Atmosphere performs very well, 33 which shows the potential of using 3D adaptive meshes in atmospheric modeling. Finally, as an alternative cut-cell 34 mesh in Fluidity-Atmosphere, the anisotropic adaptive mesh coupled with the Galerkin method provides an alternative 35 accurate representation of terrain-induced flow.

36

37 Keywords

- 38 Fluidity-Atmosphere
- 39 Dynamically Adaptive Mesh
- 40 Mountain Wave
- 41 Galerkin Method

43 **1. Introduction**

44 Atmospheric motion involves a wide range of spatial scales, from large-scale flows $O(10^6 - 10^7) m$ down to 45 parameterized turbulence $O(10^{1}-10^{2}) m$ (Kühnlein 2011; Zheng et al. 2015). In numerical weather prediction (NWP) 46 models, the straightforward way to resolve more small-scale phenomena is by using a high-resolution mesh, which 47 leads to a high computational cost. However, it is often not feasible to use a global uniform high-resolution mesh to 48 simulate large- and small-scale phenomena simultaneously with limited computational resources. In recent decades, 49 the adoption of adaptive mesh refinement has solved this bottleneck by locally increasing the mesh resolution in the 50 key domain of NWP models and leaving a coarse resolution for the rest of the model. Adaptive mesh refinement can 51 be distinguished into static and dynamic refinement (Marras et al. 2016). For static mesh refinement, resolution 52 adjustment is always achieved by hierarchical mesh nesting, which has been widely used in many NWP models: WRF 53 (Skamarock et al. 2007), GRAPES (Yang et al. 2008), COSMO (Steppeler et al. 2002; Doms and Baldauf 2018), 54 NAM (Janjic 2003), RAMS (Pielke et al. 1992), etc. For dynamic mesh refinement, the mesh is adjusted in time and 55 space, thereby enabling multiscale processes to be resolved and the features of flows to be captured as time evolves. 56 Skamarock et al. (1989) and Skamarock and Klemp (1993) first applied adaptive meshes in atmospheric sciences. 57 Bacon et al. (1999) developed the first operational adaptive model, the operational multiscale environment model with 58 grid adaptivity (OMEGA), and simulated hurricane tracks with a horizontal adaptive mesh. Iselin (2002) utilized a 59 stretched adaptive mesh to address 1D and 2D advection problems. St-Cyr et al. (2008) compared two shallow-water 60 models with quad-tree adaptive mesh refinement and demonstrated that the adaptive mesh was able to track features 61 of interest without visible distortion at the mesh interfaces. Weller et al. (2016) introduced a new r-adaptive mesh 62 using optimal transport and the numerical solution of a Monge-Ampère type equation. Furthermore, the adaptive mesh 63 has been a strong competitor in resolving multiscale dynamic and chemical processes (Garcia-Menendez and Odman 64 2011; Karamchandani et al. 2011). Odman and Khan (2002) and Odman et al. (2004) introduced adaptive mesh 65 techniques into an air quality model for an ozone case. Zheng et al. (2015) and Zheng et al. (2020) used the anisotropic 66 adaptive mesh technique to accurately represent the air pollutant transport process and chemical reactions. With the 67 rise of grid-independent Galerkin methods and finite volumes (Ford et al. 2004; Nair et al. 2005; Ahmad et al. 2006; 68 Giraldo and Restelli 2008; Giraldo and Warburton 2008; Li et al. 2008; Jablonowski et al. 2009), a number of research 69 studies on dynamic mesh adaptation combined with element-based Galerkin methods have been performed in 70 meteorology applications (Chen et al. 2011; Müller et al. 2013; Yelash et al. 2014; Kopera and Giraldo 2014). Marras et al. (2016) pointed out that element-based Galerkin methods might perform well in next-generation atmospheric and climate models competing with finite difference and spectral transform methods. Savre et al. (2016) first introduced the anisotropic adaptive mesh technique into atmospheric modeling in both horizontal and vertical directions and evaluated it with 2D idealized test cases.

75 In this study, we develop a new 3D dynamically adaptive atmospheric model (Fluidity-Atmosphere) based 76 on the dynamic framework of Fluidity, a computational fluid dynamic (CFD) model developed by the Applied 77 Modeling and Computation Group (AMCG), Imperial College London (ICL) (Pain et al. 2001, 2005; Piggott et al. 78 2009). Its accuracy and conservation properties have been validated by a series of idealized simulations using a 79 uniform mesh, and the computational cost has been decreased by mesh adaptivity in rising bubble, density current and 80 interacting warm and cold bubble tests (Pain et al. 2001, 2005; Piggott et al. 2009; Savre et al. 2016; Zheng et al. 81 2015; 2020). Fluidity-Atmosphere applies dynamically tetrahedral adaptive meshes in 3D space and time so that 82 regions of steep topography, high dynamic activity or specific interest can be modeled with high horizontal and vertical 83 resolutions. The tetrahedral (triangular in 2D) mesh can be adapted in an anisotropic way so that the mesh refinement 84 works on a targeted domain with preferential research requirements (for example, strong convections or local turbulent 85 flows). The adaptive mesh is combined with a range of control volumes and finite element discretization methods to 86 optimally represent flows (e.g., tracers and temperature). With mesh adaptivity, the mass is conserved by a supermesh 87 interpolation strategy (Farrell et al. 2009).

88 In atmospheric modeling, the computational mesh plays an important role in topographical representation, 89 which is vital for accurately simulating mountain waves and the pressure gradient force. Currently, terrain-following 90 coordinates (Phillips 1957; Gal-Chen and Somerville 1975) are widely used in many NWP models for topographical 91 representation. However, in the vicinity of steep mountains, the nonorthogonality of terrain-following coordinates 92 leads to spurious winds and significant pressure gradient force errors (Sundqvist 1976; Good et al. 2014; Nishikawa 93 and Satoh 2016; Li et al. 2016a). This can be improved, for example, by topographical smoothing with height (Schär 94 et al. 2002; Leuenberger et al. 2010; Klemp 2011; Li et al. 2014) and improvements in the accuracy of schemes for 95 computing the pressure gradient force (Zängl 2012; Li et al. 2012; Weller and Shahrokhi 2014; Li et al. 2016b). Even 96 so, errors are inevitably introduced on ground with unmodified steep terrain in a high-resolution model (Shaw and 97 Weller 2016). An alternative topographical representation is the cut-cell method (Steppeler et al. 2002; Yamazaki and 98 Satomura 2010; Lock et al. 2012; Good et al. 2014). Cut cells and the Galerkin method have in common that the

99 representation of the mountains is achieved by adapting the computational mesh rather than by coordinate 100 transformation. The thin-wall approximation (Steppeler et al. 2002) and grid emerging technique (Yamazaki and 101 Satomura 2010) improved computational efficiency and numerical stability. Steppeler et al. (2006, 2011, 2013, 2019) 102 demonstrated improvements in the prediction of precipitation and potential temperature by the cut-cell method 103 compared with the terrain-following method. Lock et al. (2012) extended a 3D cut-cell approach for steep mountains 104 using piecewise bilinear surfaces. Gallus and Klemp (2000) found that the step-mountain method, representing terrain 105 by a piecewise constant function, can lead to a lack of convergence and artificial flow separation, which cannot even 106 be repaired by a very high vertical resolution. It turned out that representing a mountain by a continuous piecewise 107 linear spline avoids the mentioned difficulties of the step-mountain approach. In Fluidity-Atmosphere, the terrain is 108 embedded within a tetrahedral (triangular in 2D) mesh, similar to the cut-cell method. By specifying the mesh aspect 109 ratio and gradation (smoothness), the flexible mesh adaptivity technique avoids the use of small-size cut cells, thus 110 allowing a large time-step size while maintaining numerical stability.

111 The performance of Fluidity, including the approximation accuracy, numerical stability, mesh convergence 112 and conservation properties, has been demonstrated by Pain et al. (2001), (2005); Farrell et al. (2009); Piggott et al. 113 (2009); Savre et al. (2016); Li et al. (2018); and Zheng et al. (2015), (2020). One important unanswered question is 114 whether Fluidity-Atmosphere can accurately represent the underlying terrain and simulate mountain waves, which 115 have a dominant effect on atmospheric motions as the horizontal resolution approaches or exceeds $O(10^1)$ km (Gallus 116 and Klemp 2000). We conduct a sequence of 2D nonhydrostatic mountain wave tests to evaluate the performance of 117 Fluidity-Atmosphere and then extend them to 3D. In Sect. 2, we introduce the characteristics, governing equations 118 and numerical schemes of Fluidity-Atmosphere. In Sect. 3, we provide the theory of anisotropic adaptive mesh 119 techniques in Fluidity-Atmosphere. In Sect. 4, the performance of adaptive unstructured meshes is tested through a 120 series of 2D and 3D experiments. Sect. 5 evaluates the ability of Fluidity-Atmosphere to accurately represent the 121 underlying terrain. Finally, the conclusions and discussion are presented in Sect. 6.

123 **2.** Description of the Fluidity Atmosphere: A Dynamically Adaptive Atmospheric Dynamic

124 Framework

In this work, the dynamic framework of Fluidity-Atmosphere is based on a set of equations within Fluidity (developed by AMCG, ICL), consisting of the continuity equation, nonhydrostatic momentum equation, and energy budget equation. Fluidity has the following features:

- Anisotropic tetrahedral adaptive meshes in 3D space and time such that regions of steep topography,
 high dynamic activity or specific interest can be modeled with high horizontal and vertical resolutions;
 - A range of control volumes and continuous and discontinuous finite element discretization methods;
- Finite element types ($P_N P_M$, where P is a polynomial and N and M are the degrees of the polynomials for velocity and pressure, respectively) designed to optimally represent flows (e.g., tracers and temperature);
- Conservative mesh-to-mesh interpolation;
- 135 Parallel computing.
- 136

140

130

137 **2.1 Governing Equations**

138For meteorological applications, the continuity equation, nonhydrostatic momentum equation, energy budget139equation, and atmospheric state equations are taken into account as follows:

$$\frac{\partial \rho}{\partial t} = -\nabla \cdot \left(\rho \vec{u} \right) \,, \tag{1}$$

141
$$\frac{\partial u}{\partial t} = -\vec{u} \cdot \nabla \vec{u} - \frac{1}{\rho} \nabla p - \vec{g} - f \vec{k} \times \vec{u} + \vec{D}_{\vec{u}} , \qquad (2)$$

-

142
$$\frac{\partial \Theta}{\partial t} = -\nabla \cdot \left(\vec{u} \Theta \right) - \rho w \frac{\partial \theta_0}{\partial z} + S_\Theta + D_\Theta , \qquad (3)$$

143
$$p = p_0 \left(\frac{\rho R_d \theta}{p_0}\right)^{\gamma} , \qquad (4)$$

144 where
$$\nabla = \frac{\partial}{\partial x}\vec{i} + \frac{\partial}{\partial y}\vec{j} + \frac{\partial}{\partial z}\vec{k}$$
, *t* represents the time, ρ is the dry density, $\vec{u} = (u, v, w)^T = (u_1, u_2, u_3)^T$ is the

145 velocity vector, p is the pressure ($p(x, y, z) = p_0(z) + p'(x, y, z)$, where the subscript '0' represents the basic

146 state of the corresponding variable with respect to z and p' is the perturbation of pressure), \vec{g} is the acceleration of

147 gravity, f represents the inertial Coriolis force, $\Theta = \rho \theta - \rho_0 \theta_0$ is the perturbation of potential temperature,

148
$$\gamma = \frac{c_p}{c_v} = 1.4$$
 is the ratio of the heat capacities for dry air, $R_d = 281J \cdot kg^{-1} \cdot K^{-1}$ is the gas constant for dry air,

149 S_{Θ} refers to the source term of the energy budget equation and $\vec{D}_{\vec{u}}$ and D_{Θ} are the subgrid turbulent mixing terms, 150 defined as:

151
$$D_{u_i} = \frac{\partial}{\partial x_j} \left[K_M \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \right], \qquad (5)$$

152
$$D_{\Theta} = \frac{\partial}{\partial x_j} \left(K_H \frac{\partial \Theta}{\partial x_j} \right), \tag{6}$$

153 where x_j represents the x-, y- and z-axes (j = 1, 2, 3), K_H is the diffusivity and K_M is the viscosity.

2.2 Discretization of the Governing Equations

155 Fluidity-Atmosphere employs the mixed continuous/discontinuous Galerkin method for spatial 156 discretization, and a time-stepping λ scheme is adopted for temporal discretization (here, the Crank-Nicolson scheme 157 with $\lambda = 0.5$). For details of the characteristics and numerical schemes in Fluidity-Atmosphere, see AMCG (2014). 158 Here, we outline the discretization of the equations in Fluidity-Atmosphere. In a finite-element expansion, 159 the velocity components u, v, w and pressure are represented as

160
$$u_i(X) = \sum_{j=1}^{\aleph} N_{i,j}(X) u_{i,j} , \qquad (7)$$

161
$$p(X) = \sum_{j=1}^{N} M_j(X) p_j$$
, (8)

162 and the perturbation of potential temperature Θ is:

163
$$\Theta(X) = \sum_{j=1}^{N} N_{\Theta,j}(X) \Theta_j , \qquad (9)$$

where $j \in \{1, 2, ..., \aleph\}$, X is the location of a node; N, M and N_{Θ} are basis functions for the velocity, pressure and perturbation of potential temperature, respectively; $u_{i,j}$, p_j , Θ_j with the subscript 'j' represent the values of the corresponding variables at node *j*; and \aleph is the total number of nodes. Note that in this study, we choose to make the continuity equation test functions the same as the pressure basis functions.

168 2.2.1 Discretized Momentum Equations

By applying finite elements, the momentum equations are tested with the velocity basis functions $\vec{N}_i = (N_u, N_v, N_w)$. By applying the λ time-stepping method and taking Eqs. (7) ~ (8) into account, the discrete momentum equations in space can be written in matrix form:

172
$$\frac{\mathbf{M}_{\mathbf{U}}}{\Delta t} \left(\mathbf{U}^{n+1} - \mathbf{U}^{n} \right) + \mathbf{A} \left(\mathbf{U}^{n+\lambda_{\mathbf{U}}} \right) \mathbf{U}^{n+\lambda_{\mathbf{U}}} + \mathbf{C} \mathbf{p}^{n+1} + \mathbf{B} + \mathbf{Cor} \mathbf{U}^{n+\lambda_{\mathbf{U}}} = s_{\mathbf{U}} , \qquad (10)$$

173 where
$$\mathbf{M}_{\mathrm{U}} \left(M_{\mathrm{U},ij} = \int_{\Omega} \rho \vec{N}_{i} \cdot \vec{N}_{j} d\Omega \right)$$
, and Ω represents the computational domain) denotes the velocity mass

174 matrix;
$$\mathbf{A}(\mathbf{U}^{n+\lambda_{\mathbf{U}}})$$
 ($A_{ij} = \int_{\Omega} \vec{N}_i \cdot (\rho \vec{u} \cdot \nabla \vec{N}_j) d\Omega$) is the advection matrix in the momentum equation; \mathbf{C}

175 $(C_{ij} = \int_{\Omega} \vec{N}_i \cdot \nabla M_j d\Omega)$ is the pressure gradient matrix; **B** $(B_i = \int_{\Omega} \rho \vec{N}_i \cdot \vec{g} d\Omega)$ is the gravity matrix; **Cor**

176 (
$$Cor_{ij} = \int_{\Omega} \rho \vec{N}_i \cdot (2\vec{\Omega} \times \vec{N}_j) d\Omega$$
) is the Coriolis force matrix; $\mathbf{U} = (\vec{u}_1, \vec{u}_2, ..., \vec{u}_N)^T$ and

177
$$\mathbf{p} = (p_1, p_2, ..., p_{\aleph})^T$$
 are vectors that contain the solutions of the velocity components and pressure over the domain
178 Ω , respectively; s_U is the source term including the diffusion terms and boundary conditions; and
179 $\mathbf{U}^{n+\lambda_U} = \lambda_U \mathbf{U}^{n+1} + (1 - \lambda_U) \mathbf{U}^n$ (where $0 \le \lambda_U \le 1$).

180 2.2.2 Discretized Continuity Equation and Pressure Correction

181 By multiplying the continuity equation with the pressure basis functions M_i and integrating it over the domain, 182 the discrete continuity equations in space can be written in matrix form:

183
$$\mathbf{M}_{\rho} \frac{\Delta \mathbf{\rho}^{n}}{\Delta t} + \mathbf{L} \mathbf{U}^{n} = \mathbf{M}_{b} q \quad , \tag{11}$$

184 where
$$\mathbf{\rho} = (\rho_1, \rho_2, ..., \rho_{\aleph})^T$$
; $M_{\rho,ij} = \int_{\Omega} N_{\rho,i} d\Omega$; $L_{ij} = \int_{\Omega} \vec{N}_i \cdot \nabla (\rho N_{\rho,j}) d\Omega - \int_{\partial\Omega} \rho N_{\rho,j} \vec{N}_i \cdot \vec{n} d\Omega$;

185 $M_{b,ij} = \int_{\partial\Omega} \rho N_{\rho,j} \vec{N}_i \cdot \vec{n} d\Omega$ and $q = \vec{u} \cdot \vec{n}$, where $\partial\Omega$ represents the boundary over Ω such that the boundary

186 conditions are applied and the unit vector n is assumed to be the outward facing normal vector to the domain Ω . For 187 a given initial pressure or the pressure from the previous time level, an intermediate velocity \mathbf{u}_{*}^{n+1} can first be solved 188 using Eq. (10). By taking into account Eqs. (10) and (11), the pressure is then corrected using:

189
$$\mathbf{L}\mathbf{M}_{\mathrm{U}}^{-1}\mathbf{C}\Delta\mathbf{p}^{n+1} = \frac{\mathbf{L}\mathbf{u}_{*}^{n+1} - \mathbf{M}_{b}q}{\Delta t} + \mathbf{M}_{\rho}\frac{\Delta\boldsymbol{\rho}^{n+1}}{\left(\Delta t\right)^{2}} .$$
(12)

190 The updated pressure is substituted into Eq. (10), and the velocity is recalculated. The combination of determining the 191 momentum and correcting the pressure has to be repeated during the nonlinear iteration procedure until the solutions 192 satisfy both the continuity and momentum equations.

193 2.2.3 Discretization of the Energy Budget Equations

194 The discretized form of Eq. (3) at time level n+1 using finite elements and the λ -method is written in a 195 general way as:

196
$$\mathbf{M}_{\mathbf{F}} \frac{\mathbf{F}^{n+1} - \mathbf{F}^{n}}{\Delta t} + \mathbf{A} \left(\mathbf{U}^{n+\lambda_{\mathbf{F}}} \right) \mathbf{F}^{n+\lambda_{\mathbf{F}}} = \mathbf{s}_{\mathbf{F}} , \qquad (13)$$

197 where
$$\mathbf{F} = (F_1, F_2, ..., F_{\aleph})^T$$
, $F = \Theta$, $M_{\mathbf{F}, ij} = \int_{\partial \Omega} N_{F, i} N_{F, j} d\Omega$, $\mathbf{s}_{\mathbf{F}}$ is the source term, the diffusion terms and

198 the boundary conditions, and $\lambda_{\mathbf{F}} \in [0,1]$, where the term $\mathbf{F}^{n+\lambda_{\mathbf{F}}}$ is given by

199
$$\mathbf{F}^{n+\lambda_{\mathbf{F}}} = \lambda_{\mathbf{F}} \mathbf{F}^{n+1} + (1 - \lambda_{\mathbf{F}}) \mathbf{F}^{n} .$$
 (14)

- 200 In Fluidity-Atmosphere, the time-marching algorithm employed uses a nonlinear iteration scheme (AMCG
- 201 2014). The time loop is repeated either a fixed number of times or until convergence is achieved. Fig. 1 shows the
- 202 sequence of steps in the iteration loop.
- 203



Fig. 1 Time loop of Fluidity-Atmosphere. Note that the variables with wavy lines represent the tentative quantities during the nonlinear iterations for the variables at the next timestep. At the final nonlinear iteration,

209 3. Introduction of Anisotropic Mesh Adaptive Techniques in Fluidity-Atmosphere

In traditional atmospheric models, adaptive mesh refinement (a locally nested static mesh method) is often used to refine the mesh in local regions. In this work, we introduce an optimization-based adaptive mesh technique (Pain et al. 2001) for atmospheric modeling in both horizontal and vertical directions. Using the optimization-based adaptive technique, the anisotropic unstructured mesh can be dynamically adapted (in time and space) to resolve multiscale flow features as the flow evolves and can capture the details of flows in all three directions (Pain et al. 2001, 2005; Piggott et al. 2009). The mesh adaptivity in Fluidity-Atmosphere is achieved in four steps:

- (i) Step 1: Create a one-to-one mapping between the tetrahedral mesh elements $\{e\}$ and the Riemann metric
- 217 tensor $\overline{\mathbf{M}}$.

(ii) Step 2: Visit all the elements in turn to gauge the mesh quality with the mesh-quality function \Im .

(iii) Step 3: Apply the optimization operations in the vicinity of the meshes to improve the mesh quality. The
 operations include edge collapse, edge splitting, face-to-edge and edge-to-face swapping, edge swapping and
 node movement.

(iv) Step 4: Interpolate all the information of the variables at the original meshes into the new meshes after
 mesh adaptivity.

In Step 1, the Riemann metric tensor used to guide the adaptive meshing algorithm can be defined as

225
$$\overline{\mathbf{M}} = \frac{\gamma}{\varepsilon} \|\mathbf{H}\|$$
, (15)

where ε is the required level of error defined by users, γ is an O(1) scalar constant (here, we use $\gamma = 1$) and $\mathbf{H} = \nabla^T \nabla f$ is the Hessian matrix of the state field *f* that we seek for optimization. The Hessian matrix can be decomposed as

 $H = V_{\rm H} S_{\rm H} V_{\rm H}^{\rm T} , \qquad (16)$

230 where the matrices $\mathbf{V}_{\mathbf{H}}$ and $\mathbf{S}_{\mathbf{H}} = diag(\lambda_i^{\mathbf{H}})$ contain the eigenvectors \mathbf{e}_i and eigenvalues $\lambda_i^{\mathbf{H}}$ of the Hessian

231 matrix **H**, respectively. Then, the operator $\| \cdot \|$ for **H** is defined as:

232
$$\|\mathbf{H}\| = \mathbf{V}_{\mathbf{H}} diag\left(\left|\lambda_{i}^{\mathbf{H}}\right|\right) \mathbf{V}_{\mathbf{H}}^{T} .$$
(17)

233 To represent small-scale dynamics, a relative error metric formulation is utilized:

234
$$\overline{\mathbf{M}} = \frac{\gamma \|\mathbf{H}\|}{\max\left(|\boldsymbol{\sigma}| \cdot |\boldsymbol{f}|, |\boldsymbol{\sigma}_{\min}|\right)} , \qquad (18)$$

where *f* is the field under consideration, σ is now a relative tolerance, and σ_{\min} is the minimum tolerance used to ensure that the denominator never becomes zero. To further control the quality of mesh adaptivity, we can impose some suitable tolerances on the interpolation errors and set restrictions, for example, the minimum and maximum element sizes and aspect ratio, on the mesh. It is also very useful to specify heterogeneous, anisotropic minimum and maximum element sizes for the adaptive mesh.

240 In Step 2, the mesh quality function is defined as:

241
$$\Im = \sqrt[p]{\sum_{e=1}^{\aleph} (\Im_e)^p} = \sqrt[p]{\sum_{e=1}^{\aleph} \left[\frac{1}{2} \sum_{l \in \ell_e} (\alpha_l)^2 + (q_e)^2 \right]^p} , \qquad (19)$$

where *p* is the index of the norm used, *l* is the edge of element *e*, α_l is a variable used to gauge the deviation of the mesh size compared with a regular tetrahedron, and q_e is a quantity used to evaluate the deviation of the mesh shape compared with a regular tetrahedron with respect to the metric tensor $\overline{\mathbf{M}}$.

In Step 3, the operations of mesh optimization will visit every element in turn and obtain the new computational mesh, then gauge the mesh quality. To determine whether mesh adaptation is executed, we list the criteria for grid refinement:

248
$$\max_{e} \left\{ \mathfrak{I}_{e} \right\} - \max_{e'} \left\{ \mathfrak{I}'_{e'} \right\} \leq -\kappa, \max_{e} \left\{ \mathfrak{I}_{e} \right\} > \mathfrak{I}_{\varepsilon} , \qquad (20)$$

249
$$\max_{e} \{\mathfrak{T}_{e}\} - \max_{e'} \{\mathfrak{T}'_{e'}\} \le 0, \frac{1}{\aleph} \max_{e} \{\mathfrak{T}_{e}\} - \frac{1}{\aleph'} \max_{e'} \{\mathfrak{T}'_{e'}\} \le -\kappa, \max_{e} \{\mathfrak{T}_{e}\} > \mathfrak{T}_{\varepsilon}, \qquad (21)$$

where \mathfrak{I}_{e} and $\mathfrak{I}'_{e'}$ are the original and newly generated mesh-quality functions, \mathfrak{I}_{e} is a certain threshold value 250 251 (here, we use 0.15), and κ is a controlling parameter. If either Eq. (20) or Eq. (21) is satisfied, mesh adaptation will 252 be implemented. Otherwise, the mesh returns to the previous status. 253 In Step 4, a mass-conserving interpolation approach, the Galerkin projection (Farrell et al. 2009; Savre et al. 254 2016), is utilized to interpolate solutions from the previous mesh to the newly generated adaptive mesh, which is 255 implemented by a supermeshing algorithm. For the details of the grid adaptivity measurements, we refer to AMCG 256 (2014). 257 258 4. Idealized Mountain Wave Test Cases 259 In this section, the performance of Fluidity-Atmosphere using anisotropic adaptive unstructured meshes is 260 evaluated with three test scenarios: 261 (i) nonhydrostatic flow in a stable stratified atmosphere around a 2D bell-shaped mountain (Lock et al. 2012); 262 (ii) sensitivity analysis of the mountain wave results with respect to different adaptive mesh sizes in the 263 horizontal and vertical directions; 264 (iii) a sequence of experiments simulating nonhydrostatic flow over the 3D steep bell-shaped hill specified in 265 Lock et al. (2012); 266 Here, the dynamically adaptive mesh technique ensures computational effort in resolving the dynamic flow process 267 over a wide range of spatial scales. 268 269 4.1 2D Adaptive Nonhydrostatic Mountain Wave 270 In this test, we use the benchmark 2D test of Lock et al. (2012) for flow over a bell-shaped mountain with 271 steady boundary conditions to form a stable upward-propagating mountain wave in a stratified atmosphere. 272 The computational domain is 60 km wide in the horizontal direction and 16 km deep in the vertical direction, 273 with a simulation time of 50000 s. The timestep is set to 5.0 s, and mesh adaptation is performed every 10 timesteps. 274 The anisotropic gradation and maximum aspect ratio are restricted to 2 and 10, respectively. Before the actual 275 simulation starts, the mesh is adapted twice to capture the basic information of the initial fields. The resolution of the 276 adaptive meshes varies from 0.2 km to 2 km with respect to the solution of the state variables (the velocity vector here), while the absolute interpolation error is set to 0.1 in the horizontal direction and 0.02 in the vertical direction. For comparison purposes, the control run is conducted in a fixed mesh with horizontal and vertical resolutions of dx = dz $= 0.2 \ km$ (Fig. 4).

For spatial discretization, continuous Galerkin (CG) and control volume (CV) methods are applied. The basis functions *N*, *M* and N_{Θ} used to approximate the velocity, pressure and perturbation of the potential temperature are first order. For the CV method, the face value is obtained by first-order upwind discretization or alternatively by using finite element interpolation (hereafter referred to as CV1 and CV2, respectively, AMCG, 2014). For temporal discretization, we utilize the semi-implicit Crank-Nicolson scheme with $\lambda = 0.5$.

285 The underlying 2D bell-shaped mountain is defined as:

286
$$h(x) = \frac{h_0}{1 + \frac{x^2}{a^2}},$$
 (22)

where $h_0 = 400m$ is the maximum height of the mountain and the half-width of the mountain is a = 1000m. We use a constant Brunt-Väisälä frequency of $N = 0.01s^{-1}$ to define the stratified background, and the bottom potential temperature is $\theta_0 = 293.15K$. The initial velocity of the flow is $\vec{u} = (10,0)^T m/s$. We apply no-flux boundary conditions along the bottom surface. Open lateral boundary conditions are used at the inflow and outflow boundaries. Since $\frac{Na}{u} = 1$, this test belongs to the nonhydrostatic range based on the analysis in Gallus and Klemp (2000). To prevent the oscillation of the waves reflected at the top and the lateral boundaries, an absorbing layer is

added on the top of the model, and strong diffusion is included at the lateral boundaries. In the outermost $z_s = 6km$

294 at the top of the model, a damping coefficient α is set after the prediction at the *n*-th time step:

295
$$\alpha = \begin{cases} -\alpha_{\max} \left[1 - \cos\left(\frac{\pi}{2} \frac{z - z_s}{z_{top} - z_s}\right) \right], \text{ for } z_s < z < z_{top}, \\ 0, & \text{otherwise.} \end{cases}$$
(23)

296 where $z_{top} = 16km$ such that the damped model solutions ϕ (including u, v, w, Θ) at the *n*-th time step become:

297
$$\phi_n = \phi_n^0 + \alpha \left(\phi_n^0 - \phi_0 \right) , \qquad (24)$$

298 where ϕ_0 is the initial state of the variable ϕ and ϕ_n^0 is the variable after the *n*-th time step without damping. Here, 299 $\alpha_{\text{max}} = 1$.

300 For stability, we define two continuous diffusions K_L and K_V , where K_L is the diffusion for the lateral

301 boundaries:

302
$$K_{L} = \begin{cases} K_{L}^{\max}, & \text{for } x_{out} < x < x_{b}, \\ K_{L}^{\max} \frac{x - x_{in}}{x_{out} - x_{in}}, & \text{for } x_{in} < x < x_{out}, \\ 0, & \text{otherwise}, \end{cases}$$
(25)

303 and K_V is the diffusion in the vertical direction:

304
$$K_{V} = \begin{cases} K_{V}^{\max}, & \text{for } z_{bot} < z < z_{a}, \\ K_{V}^{\max} \frac{z_{b} - z}{z_{b} - z_{a}} + K_{V}^{\min}, & \text{for } z_{a} < z < z_{b}, \\ 0, & \text{otherwise,} \end{cases}$$
(26)

where $K_{H}^{\text{max}} = 50000m^{2} / s$; x_{in} and x_{out} are the innermost and outermost positions for using diffusion, in which the diffusion ranges linearly from 0 to K_{H}^{max} ; and x_{b} is the position of the boundaries. Here, $[x_{in}, x_{out}, x_{b}] = [10, 6, 0]km$ at the inflow boundary and [50, 54, 60]km at the outflow boundary. $K_{V}^{\text{max}} = 500m^{2} / s$ and $K_{V}^{\text{min}} = 100m^{2} / s$; $z_{a} = 3km$ and $z_{b} = 4km$ are the starting and ending boundaries for the linear range of K_{V} in the vertical direction from K_{V}^{min} to K_{V}^{max} , and $z_{bot} = 0$. Thus, the diffusion is defined as:

 $K = K_L + K_V (27)$



312

Fig. 2 Vertical velocity solution for the mountain wave simulation over a 2D bell-shaped terrain with a contour interval of 0.25 *m/s*. (a): The analytic solution reproduced from Gallus and Klemp (2000); (b) and (c): the solutions of the CV1 method; (d) and (e): the solutions of the CV2 method; (f) and (g): the solutions of the CG method. (b), (d) and (f) are for a fixed mesh, while (c), (e) and (g) are for an adaptive mesh.

Fig. 2 illustrates the contours of the vertical velocity until a steady-state velocity is achieved by (a) linear theory (Gallus and Klemp 2000); (b), (e) CV1; (c), (f) CV2; and (d), (g) CG. The analytic solution is obtained using Eq. (4) with linear theory for a flow past the step mountain of Gallus and Klemp (2000). The left and right columns are the results for fixed and adaptive meshes, respectively. All the flow patterns using Fluidity-Atmosphere show good 322 agreement with the analytic solution, and the contours of the vertical velocity are stacked vertically above the terrain. 323 A comparison between the results for the fixed mesh and the adaptive mesh reveals that the adaptive mesh is able to 324 simulate mountain waves with a similar quality as the fixed mesh. The deviations from the analytic solution with 325 respect to the magnitude of the vertical velocity among CV1, CV2 and CG exhibit a declining trend. The CV1 method 326 (Fig. 2b and 2c) shows a smaller velocity farther from the peak of the mountain because the first-order upwind scheme 327 is less accurate. The pattern and center position of the wave in CV2 (Fig. 2d and 2e) and CG (Fig. 2f and 2g) are 328 comparable to those of the analytic solution (Fig. 2a). Moreover, the results for the fixed mesh exhibit smooth vertical 329 velocity contours, while a few numerical artifacts can be detected at the periphery of the contours (e.g., the outermost 330 contour) for all the adaptive-mesh cases. This may be seen as a small error arising from adaptivity.





Fig. 3 Horizontal velocity solution and the corresponding adaptive mesh for the mountain wave simulation over a
2D bell-shaped terrain with a contour interval of 0.2 *m/s*. The left column contains all the results for the fixed mesh,
while the right column shows those of the adaptive mesh. (a) and (b): The solutions of the CV1 method; (c) and (d):
the solutions of the CV2 method; (e) and (f): the solutions of the CG method.

Fig. 3 shows the horizontal velocity contours. Small artificial noise in the vicinity of the mountain at a height of almost 1 *km* occurs with the adaptive mesh cases. The spurious oscillation on the entire bottom boundary is incorrectly captured by the adaptive meshes and is thus artificially amplified in the vicinity of the mountain. This can be observed correspondingly for the adaptive mesh snapshot in Fig. 4.





Fig. 4 Computational meshes for the mountain wave simulation over a 2D bell-shaped terrain. (**a**): Terrain-following triangular fixed meshes with dx = dz = 200 m; (**b**), (**c**) and (**d**): anisotropic adaptive meshes with the CG, CV1 and CV2 methods. The maximum and minimum lengths are 2000 *m* and 200 *m*. (**e**) and (**f**) show the magnified views of (**a**) and (**b**) marked by the blue rectangular areas.

Compared with the CG results, the CV1 and CV2 methods possess an intrinsic viscosity (diffusion). Although an increase in K_{ν}^{max} makes the numerical noise disappear, it is accompanied by a reduction in the magnitude of the velocity. Therefore, in order to eliminate the noise around the peak of the mountain and maintain the magnitude of the velocity, partial node locking at the bottom boundary will be conducted in Sect. 5.

Number of Cells/Points	Spatial Discretization	Fixed Mesh	Adaptive Mesh			
			Start $(t = 0 s)$	Steady ($t = 50000 \ s$)		
	CV1	48000	1447	6064		
Cells	CV2	48000	1447	8914		
	CG	48000	1447	9596		
	CV1	24381	644	3132		
Points	CV2	24381	644	4560		
	CG	24381	644	4901		

Table 1 The number of cells and points used for the fixed mesh and the adaptive mesh in Sect. 4.1.

356 The relationship between the mesh refinement and computational costs for the fixed mesh and the adaptive 357 mesh was investigated. The meshes for the simulation are shown in Fig. 4, and the number of cells and points and the 358 corresponding ratios of the adaptive mesh and the fixed mesh are provided in Tabs. $1 \sim 2$. The fixed mesh is composed 359 of triangular meshes based on terrain-following quadrilaterals that are cut into two triangles by one diagonal line. The 360 numbers of cells and points in the fixed mesh are constant values of 48000 and 24381, respectively. In contrast, the 361 adaptive mesh changes every 10th timestep, so we present the numbers at the start time and at the time when the steady 362 solution is reached. We note that the mesh is adapted with respect to the velocity such that the entire domain is filled 363 with coarse meshes before the activation of the mountain wave. Then, at the steady state, the wave continuously 364 propagates downstream and upward from the peak of the mountain, leading to a high-resolution dense mesh 365 aggregated on the entire leeward side of the mountain. Due to the decay of the velocity magnitude with height, the 366 mesh becomes coarser than the mesh in the vicinity of the mountain, as shown in Figs. $4b \sim 4d$. The mesh adaptivity 367 therefore reduces the number of cells and points to $6064 \sim 9596$ and $3132 \sim 4901$. The corresponding ratio of the 368 adaptive mesh and the fixed mesh becomes 12.7% for CV1, 18.6% for CV2 and 20% for CG. The ratio of runtimes 369 between the adaptive mesh and the fixed mesh is proportional to the ratio of the number of nodes and cells. Therefore, 370 to achieve the desired accuracy, the adaptive mesh requires fewer computational nodes and a shorter runtime through 371 the whole domain, thus improving the computational efficiency compared to the fixed mesh. Moreover, for the 372 adaptive mesh, the difference in accuracy in the vertical velocity among CV1, CV2 and CG can be reflected by the 373 difference in the number of cells and points in these test cases. In other words, the greater the number of cells and 374 points, the higher the accuracy achieved.

376 **Table 2** Three ratios of the adaptive mesh and the fixed mesh at t = 50000 s from the six mountain wave tests presented

377 in Sect. 4.1.

Ratio	CV1	CV2	CG
Number of Cells	12.63%	18.57%	19.99%
Number of Points	12.85%	18.70%	20.10%
Runtime	13.11%	18.28%	23.56%

378

379

4.2 2D Adaptive Nonhydrostatic Mountain Wave with Different Resolutions and the Relation 380 to the Cut Cells

381 Our study now focuses on the resolution dependence of mountain wave modeling using adaptive mesh 382 techniques. In this study, the simulations of the mountain wave are set up as in Sect. 4.1 except for the setting of the 383 adaptive meshes. Since the performance of the CG method is superior to that of the CV methods, CG will be utilized 384 in the following tests. To evaluate the impact of the horizontal (vertical) resolution, we keep the minimum vertical 385 (horizontal) mesh size at 200 m, while the minimum horizontal (vertical) mesh size is 1600, 800, 400, 200, 100 and 386 50 m.

387 The results with variations in the horizontal mesh size are shown in Fig. 5. These results (the accuracy and 388 location of the wave contours) agree well with the analytic solution except for those for the coarse mesh scheme. 389 According to the increase in the horizontal mesh resolution, the amplitudes of the vertical velocity are increased 390 somewhat positively at the peak of the mountain, and the contour of the vertical velocity becomes smooth, although 391 there is slight noise on the bottom boundary. However, when the mesh size is less than 200 m, the effect of increasing 392 the horizontal resolution is not obvious in terms of smoothness, and the continuity of the solution is different from the 393 results in Gallus and Klemp (2000) (Figs. 5e and 5f). This is because Fluidity-Atmosphere enables a piecewise 394 continuous mountain representation to achieve convergence, especially for high horizontal resolution.

395 In detail, the scheme in Fluidity-Atmosphere is very similar to the cut-cell formulation for the representation 396 of mountains, which is achieved by mesh adaptation instead of coordinate transformation. In fact, for the fixed mesh 397 study, the scheme in Fluidity-Atmosphere is a cut-cell formulation (using an unstructured mesh). For the unstructured 398 adaptive mesh used here, the problem of the appearance of very small cells, typical for cut cells, is not present. As a 399 mountain is represented here by piecewise linear spline results, we are free from the problems pointed out by Gallus

and Klemp (2000) for mountain representations by piecewise constant splines. This result is in full agreement with
Steppeler et al. (2002), who concluded that the problems for Gallus and Klemp (2000) disappear when the bottom
boundary is changed to a piecewise linear mountain. Furthermore, cut cells allow the presence of steep mountains,
which will be addressed in Sect. 4.3.



405

406Fig. 5 Vertical velocity solution of the mountain wave simulation over a 2D bell-shaped terrain with different407horizontal mesh sizes. The maximum mesh size in both the horizontal and vertical directions is 2000 m, and the408minimum vertical mesh size is 200 m. The minimum horizontal mesh sizes are (a) 1600 m, (b) 800 m, (c) 400 m, (d)409200 m, (e) 100 m and (f) 50 m. The contour interval is 0.25 m/s.

411 With the increase in vertical resolution shown in Fig. 6, the vertical velocity contour is near the analytic 412 solution. Similar to the result in Fig. 5a, the coarse-resolution simulation result (dz = 1600 m in Fig. 6a) exhibits very 413 strong vertical oscillations, especially for the area over the peak of the mountain. The error can be reduced by 414 increasing the vertical resolution (Figs. 6b~6d). When further increasing the vertical resolution to dz = 50 m from 200 415 m, both the smoothness and the magnitude of the contours are always preserved (Figs. $6d \sim 6f$). Combined with the 416 results in Figs. 5d ~ 5f, dx = dz = 200 m should be a wise choice for Fluidity-Atmosphere in the 2D mountain-wave 417 simulation. We note that the maximum height of the mountain is 400 m, so the increase of the vertical resolution has 418 a strong impact on the representation of the terrain when dz < 400 m. Because it is different from the step-mountain 419 coordinate, the adaptive mesh in Fluidity-Atmosphere makes the underlying terrain smoother. Therefore, judging from 420 the contours of the velocity contour, Fluidity-Atmosphere maintains its characteristics at dz = 200 m.



Fig. 6 Vertical velocity solution of the mountain wave simulation over a 2D bell-shaped terrain with different
vertical mesh sizes. The maximum mesh size in both the horizontal and vertical directions is 2000 m, and the
minimum horizontal mesh size is 200 m. The minimum vertical mesh sizes are (a) 1600 m, (b) 800 m, (c) 400 m, (d)
200 m, (e) 100 m and (f) 50 m. The contour interval is 0.25 m/s.

427

428 4.3 3D Adaptive Nonhydrostatic Mountain Wave

To demonstrate the accuracy and stability of 3D Fluidity-Atmosphere, we extend the benchmark test of Lock et al. (2012) to 3D. The computational domain is 60 km wide in both horizontal directions and 16 km deep in the vertical direction with a simulation time of 15000 s. The resolution of the adaptive meshes varies from 0.125 km to 10 km. Mesh adaptation is performed every 5 timesteps. All other parameters related to mesh adaptivity are kept the same as those in Sect. 4.1.

434 The underlying 3D bell-shaped mountain is defined as:

435
$$h(x,y) = \frac{h_0}{\left(1 + \frac{x^2 + y^2}{a^2}\right)^{\frac{3}{2}}},$$
 (22)

where $h_0 = 400m$ is the maximum height of the mountain and the half-width of the mountain is a = 1000m. The stratified background state is defined by $N = 0.01s^{-1}$, and the potential temperature at the bottom surface is $\theta_0 = 293.15K$. The initial velocity of the flow is $\vec{u} = (10,0,0)^T m/s$. To prevent the oscillation of the waves reflected at the top and lateral boundaries, the treatments for the top and lateral boundaries of the model used in Sect. 4.1 are also applied here. The stable and smooth solution is shown in Fig. 7. In Fig. 7a, the mountain wave propagates upward from

the peak of the mountain, and its strength decays with height. In the horizontal *x-y* slice at $z = 2 \ km$ (Fig. 7b), the contour of the vertical velocity is very smooth and symmetric. The same symmetric distinguishing pattern can be seen in the vertical cross-section at $x = 32 \ km$ downstream of the mountain (Fig. 7c), although slight noise appears at approximately $z = 1 \ km$. In the horizontal slice at $z = 800 \ m$ (Fig. 7d), a little noise appears in the outermost layer of the contour.





449 Fig. 7 Contours of the vertical velocity for the mountain wave simulation over a 3D bell-shaped terrain. (a) Vertical 450 cross-section through the center of the mountain at y = 30 km with a contour interval of 0.25 m/s; (c) vertical cross-451 section at x = 32 km, which is 2 km downstream of the peak of the mountain and has a contour interval of 0.1 m/s; 452 (b) and (d) horizontal cross-sections at heights z = 2000 m and z = 800 m with a contour interval of 0.1 m/s, 453

respectively.

454

455 Both results are comparable to the results of Fig. 7 in Lock et al. (2012, hereafter referred to as Lock Fig. 7), 456 although there is a little noise along the bottom due to the use of the unstructured adaptive mesh. The center positions 457 and amplitudes of the waves shown at the x-z and y-z slices are in good agreement in the vicinity of the mountain. 458 When x > 38 km, the height of the third contour of the positive vertical velocity in Fig. 7a is slightly higher than that 459 in Lock Fig. 7a. Furthermore, the magnitudes of the extreme centers at the peak of the mountain at the horizontal 460 cross-sections (z = 2000 m and z = 800 m) are consistent with those of Lock Figs. 7b and 7d. Only the maximum value 461 of the negative extreme center downstream of the mountains is slightly smaller than that of Lock Figs. 7b and 7d, 0.1 462 m/s.

Fig. 8 shows the 3D adaptive mesh in three cross-sections, which is used to capture the mountain wave features. Fig. 8c is the 3D perspective of Fig. 8a. We note that the mesh is denser in the area with higher velocity gradients and relatively sparser in the remainder of the domain.

466



468 Fig. 8 Anisotropic adaptive meshes for the vertical field for the mountain wave simulation over a 3D bell-shaped 469 terrain. (a) Vertical crinkle cross-section through the center of the mountain at $y = 30 \ km$; (b) vertical crinkle cross-470 section at $x = 32 \ km$, which is 2 km downstream of the peak of the mountain; (c) 3D perspective of (a) and (d), 471 horizontal cross-section at height $z = 2000 \ m$.

472

To further evaluate the stability and accuracy of Fluidity-Atmosphere for a steep mountain in a highresolution simulation, we conducted another test case with $h_0 = 2000m$ and a = 1000m, while the other parameters remained the same.

476 The vertical velocity of the steep mountain with $h_0 = 2000m$ and a = 1000m at t = 10000s is shown

477 in Fig. 9. For this case, the coefficient representing the nonlinearity of the flow is $\frac{Nh_0}{u} = 2 > 1$, which means that

478 the flow is strongly nonlinear (Lilly and Klemp 1979; Ikawa 1988; Gallus and Klemp 2000; Zängl et al. 2015). In this 479 situation, although the linear theory of mountain waves is invalid and the mountain waves break, the vertical velocity from the steep mountain has the same pattern as that shown in Fig. 7 with $h_0 = 400m$. Naturally, the greater height 480 481 of the mountain produces a stronger perturbation of the vertical velocity. Stacked velocity contours and a decay in 482 height at the vertical cross-section at $y = 30 \ km$ are observed. The properties of smoothness and symmetry are also 483 seen at the vertical cross-section at x = 32 km and at the horizontal cross-sections at heights z = 2000 and 4000 m. A 484 little noise at the outermost area of the contours is still detected at z = 800 m. Due to the use of adaptive meshes similar 485 to cut-cells, semi-implicit temporal discretization and the CG method, the result remains relatively stable in the case 486 of such a steep mountain.

487



488

489 Fig. 9 Contour of the vertical velocity solution for the mountain wave simulation over a 3D bell-shaped 490 terrain. (a) Vertical cross-section through the center of the mountain at y = 30 km; (b) vertical cross-section at x = 32491 km, which is 2 km downstream of the peak of the mountain; (c), (d) and (e) horizontal cross-sections at heights z =492 800, 2000, 4000 m, respectively. The contour intervals are 0.25 m/s for (a) and 0.1 m/s for all the others. The model 493 solutions are represented at t = 10000 s.

494 **5.** Accuracy of the Orographic Representation

495 The sufficient condition for accurately representing the underlying mountain in terrain-following coordinates 496 is $\Delta h < \Delta z$, where Δh and Δz are the deviation of the orographic height between two neighboring horizontal grid 497 points and the vertical resolution, respectively (Ikawa 1988; Steppeler et al. 2006). However, the ability to obtain an 498 accurate orographic representation would be hindered if the slope of the mountain became very steep or the resolution 499 of the NWP models increased. This is because the vertical resolution would be very coarse to satisfy the condition 500 $\Delta h < \Delta z$ with a large Δh for high and steep mountains. During some numerical procedures, high and steep 501 mountains may even lead to linear instability (Ikawa 1988). This error and potential instability can be removed by the 502 use of cut-cell grids or cut-cell structures. Cut-cell structures are horizontally aligned, which means that the grid lines 503 of the cells are cut into the mountain (for a review of cut-cell methods, see Steppeler et al. 2002 or Yamazaki and 504 Satomura 2010). Due to the resemblance between the adaptive mesh of Fluidity-Atmosphere and the cut-cell grid, it 505 is interesting to see whether Fluidity-Atmosphere can be used to accurately represent the terrain, thus reducing the 506 spurious wind. In this section, based on the test case in Sect. 4.1, two simulations are conducted by (i) giving a 507 perturbation of the potential temperature in the entire computational domain and (ii) using the treatment of node 508 locking in the vicinity of the mountain while keeping the other parameters identical to those in Sect. 4.1.



Fig. 10 Contour of the vertical velocity solution for the mountain wave simulation over a 2D bell-shaped terrain with a constant perturbation of the potential temperature $\Delta \theta = 5K$. The contour interval is 0.25 m/s. (a) ~ (f) show the results at t = 500, 1000, 3000, 6000, 12000 and t = 20000 s. First, we introduce an extra potential perturbation of a constant $\Delta \theta = 5K$ over the entire domain (see Saito



519 s with the CG method and a damping operation. At the beginning of the simulation, the potential temperature

520 perturbation stimulates the formation of the vertical velocity in the whole computational domain (Fig. 10a), leading

521 to the aggregation of adaptive meshes in the entire domain (Fig. 11a). With a sustained horizontal velocity (constant), 522 the impact of the potential temperature perturbation gradually becomes evanescent (Fig. 10b). At t = 3000 s, the 523 contours of the mountain wave become visible (Fig. 10c). The induced perturbations of the vertical velocity distribute 524 throughout the domain in such a way that the adaptive mesh remains dense (Fig. 11c). With the disappearance of the 525 noise at the inflow and top boundaries, the mesh is adapted to be coarse upstream of the mountain (Figs. $11d \sim 11f$). 526 Although an orographic representation error appears at the beginning, this spurious wind is reduced with the CG 527 method and the adaptive mesh of the cut-cell form in Fluidity-Atmosphere (Figs. $10d \sim f$). In the vicinity of the terrain, 528 the larger Δz (compared to Δh) inhibits the development of instability, and the adaptive grid makes the orography 529 smooth with the use of high-resolution meshes. Compared with Fig. 2g, both results are in good agreement, and the 530 features of the mountain waves are reproduced, including the stacked vertical velocity contours and the decay of the 531 strength with the height. Therefore, Fluidity-Atmosphere can accurately represent the underlying terrain and eliminate 532 the spurious winds induced by the perturbation of the potential temperature. The errors in the terrain-following 533 coordinates are reduced because the adaptive mesh forms a smoothly varying mountain in Fluidity-Atmosphere. 534



Fig. 11 The evolution of the adaptive mesh for the mountain wave simulation over a bell-shaped terrain of height 400 *m* and half-width 1000 *m* with a constant perturbation of potential temperature $\Delta \theta = 5K$. (a) ~ (f) show the results at t = 500, 1000, 3000, 6000, 12000 and t = 20000 s.

535

Second, to reduce the numerical noise near the bottom in the adaptive mesh (Figs. 2c, 2e and 2g), the mesh along the bottom boundary is locked. Furthermore, to achieve the stability condition $\Delta h < \Delta z$, we lock the terrainfollowing mesh under the height of 2000 *m* as a fixed coarse mesh with dx = dz = 200 m. All the other parameters are kept the same as those in Sect. 4.1. Because the maximum derivative of the mountain height $\frac{\partial h}{\partial x} < 0.3$ leads to

544
$$\Delta h = \frac{\partial h}{\partial x} dx < 60$$
, the condition is satisfied ($\Delta h < 60 < \Delta z$). The adaptive mesh and the contour of the velocity

545 components at
$$t = 50000 \text{ s}$$
 are shown in Fig. 12.

The noise in the vicinity of the mountain is eliminated by the node-locking treatments for both the vertical and horizontal components of the velocity using the adaptive mesh. A comparison between the fixed mesh (Figs. 2f and 3e) and the adaptive mesh with node locking (Fig. 12) reveals that the adaptive mesh is feasible for orographic representation and that the mountain wave simulation achieves the same precision with a lower computational cost than that of the fixed mesh.





Fig. 12 Contour of the velocity solution and the corresponding mesh for the mountain wave simulation over a 2D
bell-shaped terrain with node locking on the bottom boundary. (a) The horizontal velocity contour with a contour
interval of 0.2 *m/s* and (b) the vertical velocity contour with a contour interval of 0.25 *m/s* of Fluidity-Atmosphere
with the CG method.

557 6. Conclusions

In this study, we investigate the ability of the Fluidity-Atmosphere dynamic framework to simulate 3D mountain waves. In general, the 3D anisotropic adaptive and highly irregular mesh of Fluidity-Atmosphere performs well in simulations of mountain waves. The anisotropic adaptive mesh provides an alternative to capture mountain wave fronts propagating upward and downstream. The scheme used in Fluidity-Atmosphere can be seen as an adaptive and irregular mesh version of the cut-cell approach with a piecewise linear mountain representation.

563 For instance, Fluidity-Atmosphere is able to generate smooth, symmetric and stable mountain waves for the 564 flow past a bell-shaped mountain. Compared to the performance on smooth mountains (Fig. 7), Fluidity-Atmosphere 565 also performs well by almost eliminating mesh-scale oscillations on steep mountains (Fig. 9). As an alternative to the 566 cut-cell grid, the adaptive mesh coupled with the Galerkin method can eliminate the noise in the entire domain 567 introduced by the strong perturbation of the potential temperature. The characteristics of mountain waves and the 568 underlying terrain are accurately represented through automatic aggregation of the adaptive meshes. The sensitivity 569 analysis of the mesh resolution demonstrates that the variation in the horizontal and vertical resolutions has a strong 570 impact on the smoothness of the results and maintains convergence even at high resolutions. Currently, in order to 571 eliminate the noise at the bottom boundary for the simulation of mountain waves, we settled for the second-best

572	solution, which is to lock the nodes at the bottom boundary. How to choose the mesh refinement criteria to distinguish
573	noise and prognostic variables with comparable magnitudes should be taken into consideration in the future work.
574	
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580

581 Data availability statement

582 The datasets generated during the current study are available from the corresponding author on reasonable request.

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